



Mechanical response of packings of nonspherical particles: A case study of two-dimensional packings of circulo-lines

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(Received 24 May 2021; accepted 6 July 2021; published 27 July 2021)

We investigate the mechanical response of jammed packings of circulo-lines in two spatial dimensions, interacting via purely repulsive, linear spring forces, as a function of pressure P during athermal, quasistatic isotropic compression. The surface of a circulo-line is defined as the collection of points that is equidistant to a line; circulo-lines are composed of a rectangular central shaft with two semicircular end caps. Prior work has shown that the ensemble-averaged shear modulus for jammed disk packings scales as a power law, $\langle G(P) \rangle \sim P^\beta$, with $\beta \sim 0.5$, over a wide range of pressure. For packings of circulo-lines, we also find robust power-law scaling of $\langle G(P) \rangle$ over the same range of pressure for aspect ratios $\mathcal{R} \gtrsim 1.2$. However, the power-law scaling exponent $\beta \sim 0.8\text{--}0.9$ is much larger than that for jammed disk packings. To understand the origin of this behavior, we decompose $\langle G \rangle$ into separate contributions from geometrical families, G_f , and from changes in the interparticle contact network, G_r , such that $\langle G \rangle = \langle G_f \rangle + \langle G_r \rangle$. We show that the shear modulus for low-pressure geometrical families for jammed packings of circulo-lines can both increase *and* decrease with pressure, whereas the shear modulus for low-pressure geometrical families for jammed disk packings only decreases with pressure. For this reason, the geometrical family contribution $\langle G_f \rangle$ is much larger for jammed packings of circulo-lines than for jammed disk packings at finite pressure, causing the increase in the power-law scaling exponent for $\langle G(P) \rangle$.

DOI: [10.1103/PhysRevE.104.014901](https://doi.org/10.1103/PhysRevE.104.014901)

I. INTRODUCTION

Granular materials represent fascinating examples of nonequilibrium physical systems that display complex, collective behavior [1,2], such as stick-slip motion [3], shear banding [4], and segregation [5]. They are composed of discrete, macroscopic grains that interact via dissipative, frictional contact interactions. Granular materials occur in many important contexts, including numerous geological processes [6,7], food and consumer product processing [8,9], and robotics applications [10,11]. Because granular media are highly dissipative, the grains do not move unless they are driven by gravity, fluid flow, or the system boundaries. When granular systems are compressed to sufficiently large packing fractions, they become jammed and possess a nonzero static shear modulus and other solidlike properties [12].

While most dry granular materials are composed of frictional, nonspherical grains, numerous computational and theoretical studies of dry granular packings have focused on the soft-particle model in which frictionless, spherical particles interact via the pairwise, purely repulsive potential energy [13]: $U(r_{ij}) \propto (1 - r_{ij}/\sigma_{ij})^\alpha \Theta(1 - r_{ij}/\sigma_{ij})$, where r_{ij} is the separation between the centers of mass of particles i and j , σ_{ij} is their average diameter, the exponents $\alpha = 2$ and $5/2$ are

set for purely repulsive linear and Hertzian spring interactions [14], and $\Theta(\cdot)$ is the Heaviside step function that ensures the potential energy is nonzero only when the particles are in contact. For frictionless, spherical particles, the jamming transition occurs when the number of interparticle contacts, N_c , equals or exceeds the isostatic value $N_c^0 = dN - d + 1$, where d is the spatial dimension and N is the number of nonrattler particles [15]. A rattler particle has too few contacts to constrain the d_f degrees of freedom per particle. When the system is compressed above jamming onset, the pressure increases from zero and the jammed packing develops nonzero bulk and shear moduli.

A hallmark of the jamming transition in static packings of frictionless, spherical particles is that the ensemble-averaged contact number and shear modulus $\langle G \rangle$ scale as a power law in the pressure P [12,16], above a characteristic pressure P^{**} that decreases with increasing system size, as the packings are isotropically compressed above jamming onset [17]. For example, $\langle G \rangle \sim P^{1/2}$ for $P > P^{**}$ for packings of spherical particles with purely repulsive, linear spring interactions. Several previous experimental studies of compressed emulsions [18,19] and packings of thin granular cylinders [20] have also found power-law scaling of the contact number and shear modulus with pressure during isotropic compression.

In previous computational studies of packings of frictionless, spherical particles [21], we showed that there are two important contributions to the ensemble-averaged shear modulus: G_f from geometrical families and G_r from changes in the interparticle contact network during compression. For isotropic compression, jammed packings within a geometrical family are mechanically stable packings with different pressures that are related to each other by continuous, quasistatic changes in packing fraction with no changes in the interparticle contact network. G_r includes discontinuities in the shear modulus that arise from point and jump changes in the contact network [22,23]. Point changes involve the addition or removal of a single interparticle contact (or multiple contacts when a rattler particle is added or removed from the contact network) without significant particle motion. Jump changes are caused by mechanical instabilities and typically involve multiple changes in the contact network and collective particle motion.

For frictionless, spherical particles, the shear modulus along a geometrical family *decreases* with increasing pressure during isotropic compression (and no shearing of the boundaries). For systems with purely repulsive linear spring interactions, G_f decreases roughly linearly with pressure, $G_f(P)/G_0 \sim 1 - P/P_0$, where G_0 is the shear modulus at $P = 0$ and P_0 is the pressure at which $G_f(P) = 0$, although there are deviations from this simple form as the system approaches contact network changes [21,24]. Thus, the increase in the ensemble-averaged shear modulus, $\langle G \rangle$, with pressure for packings of spherical particles arises from G_r , where changes in the contact network cause discontinuous upward jumps in the shear modulus. We will show below that the sign of the second, pressure-dependent term in G_f (i.e., whether G_f increases or decreases with pressure) is determined by the curvature of geometrical families in the strain direction.

Several prior computational studies have shown that the form of $\langle G(P) \rangle$ for jammed packings depends on the particle shape [25–27]. For example, the pressure-dependent shear modulus for packings of frictionless ellipse-shaped particles with repulsive linear spring interactions scales as $\langle G(P) \rangle \sim P^\beta$, where $\beta \sim 1$ over a wide range of pressure, $P^{**} < P < P^*$, $P^{**} \sim N^{-2}$, and P^* does not depend strongly on system size. For $P > P^*$, the power-law scaling crosses over to $\langle G \rangle \sim P^{1/2}$, as found for jammed packings of spherical particles [17]. However, the ensemble-averaged shear modulus for jammed packings of dimer-shaped particles (and other composite particles formed from bonded spherical particles) scales as $\langle G \rangle \sim P^{1/2}$ over the same range of pressures and for the same aspect ratios as those studied for packings of smooth, ellipse-shaped particles [26]. Since packings of frictionless ellipse-shaped particles are hypostatic at jamming onset, while packings of dimer-shaped particles are isostatic at jamming onset, it is possible that the change in the power-law scaling exponent from $\beta = 0.5$ to ~ 1 is related to the presence of low-frequency quartic modes in the vibrational response for packings of ellipse-shaped and other nonspherical particles [28].

In addition, recent studies of the structural and mechanical properties of jammed packings of *deformable* particles that can change shape [29,30] have shown that $\langle G \rangle$ versus

P displays scaling behavior that is different from that for jammed packing packings of spherical particles. Thus, in the absence of universal behavior for the mechanical properties of jammed particle packings, it is important to develop a theoretical framework that can relate the structural and mechanical properties of single jammed configurations to the properties of the ensemble. In light of this, two important goals of the present paper are (1) emphasizing that the power-law scaling behavior of the ensemble-averaged shear modulus versus pressure depends on the particle shape and (2) describing the key ingredients—the pressure dependence of the shear modulus of geometrical families, the frequency of changes in the interparticle contact network, and the size of jumps in the shear modulus caused by the contact changes—that are needed to develop a theoretical framework for calculating the ensemble-averaged shear modulus of jammed particle packings.

Specifically, we address the question of what determines the power-law scaling exponent β for packings of nonspherical particles. Does G_f decrease with pressure for packings of nonspherical particles? Are the frequency of contact network changes and the magnitude of the discontinuities in the shear modulus at contact changes different from those for packings of spherical particles? As a case study, we investigate the pressure-dependent mechanical response of jammed packings of circulo-lines interacting via purely repulsive, linear spring interactions in two spatial dimensions as a function of aspect ratio.

We find several key results for the mechanical response of jammed packings of circulo-lines. First, the curvature of the variation of packing fraction with strain for geometrical families can be either *negative* or *positive*, and thus the shear modulus of geometrical families can either *increase* or *decrease* with pressure: $G_f/G_0 \sim 1 \pm P/P_0$ to linear order in pressure. We derive an exact expression for the pressure-dependent shear modulus of jammed packings and show that near jamming onset it can be approximated as $G_f \sim -\frac{1}{\phi} \left(\frac{dP}{d\gamma} \right)_\phi \left(\frac{d\phi}{d\gamma} \right)_P - \frac{P}{\phi} \left(\frac{d^2\phi}{d\gamma^2} \right)_\phi$ [31], where γ is the shear strain. The first term tends to a constant, $G_0 > 0$, in the zero-pressure limit and the sign of the coefficient of the second term (that is roughly linear in P) is determined by the curvature of geometric families in the ϕ - γ plane. Second, we decompose $G_f = G_a - G_{na}$ for each first, low-pressure geometrical family into its affine and nonaffine contributions. G_a gives the response of the system to a globally affine change of the particle positions and system boundaries, while G_{na} also includes particle motion in response to potential energy minimization. We find that the nonaffine term plays an important role in determining G_f . In particular, the nonaffine contribution can cause G_f to increase with pressure, which does not occur in jammed packings of spherical particles. We also calculate the ensemble-averaged shear modulus $\langle G \rangle$ versus P for jammed packings of circulo-lines over a range of aspect ratios \mathcal{R} and system sizes. For packings of circulo-lines, we find that $\langle G \rangle \sim P^\beta$, where $\beta \sim 0.8$ – 0.9 , over a range of pressures $P^{**} < P < P^*$, where $P^{**} \sim N^{-2}$ and P^* decreases as $\mathcal{R} \rightarrow 1$ and does not depend strongly on system size. We find that the finite fraction of geometrical families with negative curvature in the ϕ - γ plane causes the power-law exponent β for $\langle G \rangle$

versus P to increase compared to that for jammed packings of spherical particles.

The remainder of the article is organized as follows. In Sec. II, we describe the interparticle potential and types of contacts that occur between pairs of circulo-lines, the numerical methods used to generate jammed packings of circulo-lines, and formulas for calculating the pressure, shear stress, and shear modulus. In Sec. III, we describe the results concerning geometrical families, nonaffine contributions to the shear modulus, point and jump changes, and the ensemble-averaged shear modulus for jammed packings of circulo-lines. Finally, in Sec. IV, we provide the conclusions and point to promising future research directions. We also include an Appendix that gives explicit expressions for the affine shear modulus for packings of circulo-lines with purely repulsive, linear spring interactions.

II. METHODS

A circulo-line is the set of points that are equally distant from a line segment; it is thus a two-dimensional (2D) shape composed of a rectangular middle region capped by two semicircles on both ends. Figure 1(a) shows a circulo-line (labeled i) with diameter of the semicircles, σ_i , and length of the middle line segment, $2l_i$. We will refer to the end points of the middle line segment as the foci. The aspect ratio of a circulo-line is $\mathcal{R} = (\sigma_i + 2l_i)/\sigma_i$, and $\mathcal{R} = 1$ in the limit that the particle becomes coincident semicircles. The asphericity of a circulo-line is $\mathcal{A} = p_i^2/4\pi a_i = \frac{(2\pi+4(\mathcal{R}_i-1))^2}{4\pi(\pi+4(\mathcal{R}_i-1))}$, where $p_i = 2\pi\sigma_i + 4l_i$ is the perimeter and $a_i = \pi\sigma_i^2/4 + \sigma_i l_i$ is the area of the circulo-line. In these studies, we vary $\mathcal{R} - 1$ and $\mathcal{A} - 1$ over the ranges 10^{-2} to 2 and 10^{-5} to 0.5, respectively. We study bidisperse packings of circulo-lines to inhibit positional and orientational order. We consider packings in simulation boxes in which all of the edges have length L , periodic boundary conditions in the x and y directions, and $N/2$ large and $N/2$ small particles with end cap diameter ratio $\sigma_l/\sigma_s = 1.4$, but the same mass m and aspect ratio \mathcal{R} . To investigate the effect of system size, we studied packings with $N = 16, 64, 128, 256,$ and 512 .

In Figs. 1(b)–1(d), we show that there are three ways in which two circulo-lines can make contact (or make small overlaps) with each other: end-end, end-middle, and middle-middle contacts. Figure 1(b) shows an end-end contact between circulo-lines i and j . In this case, the relevant separation r_{ij} between the circulo-lines is the separation between the two closest foci on i and j . Another important distance is the separation λ_i between the center of circulo-line i and the point at which the line from the closest focus on j that is perpendicular to the axis of circulo-line i intersects the axis of i . For an end-end contact, the following three conditions must be satisfied: $r_{ij} < \sigma_{ij} = (\sigma_i + \sigma_j)/2$, $\lambda_i > l_i$, and $\lambda_j > l_j$.

Figure 1(c) shows an end-middle contact where the end of circulo-line j is in contact with the middle region of circulo-line i . For an end-middle contact, the relevant separation is the distance r_{ji} between the closest focus on i and the axis of j . Similarly, we can define the separation r_{ij} , but $r_{ji} \neq r_{ij}$. For an end-middle contact, the following four conditions must be satisfied: $r_{ij} < \sigma_{ij}$, $r_{ji} > \sigma_{ij}$, $\lambda_i < l_i$, and $\lambda_j > l_j$.

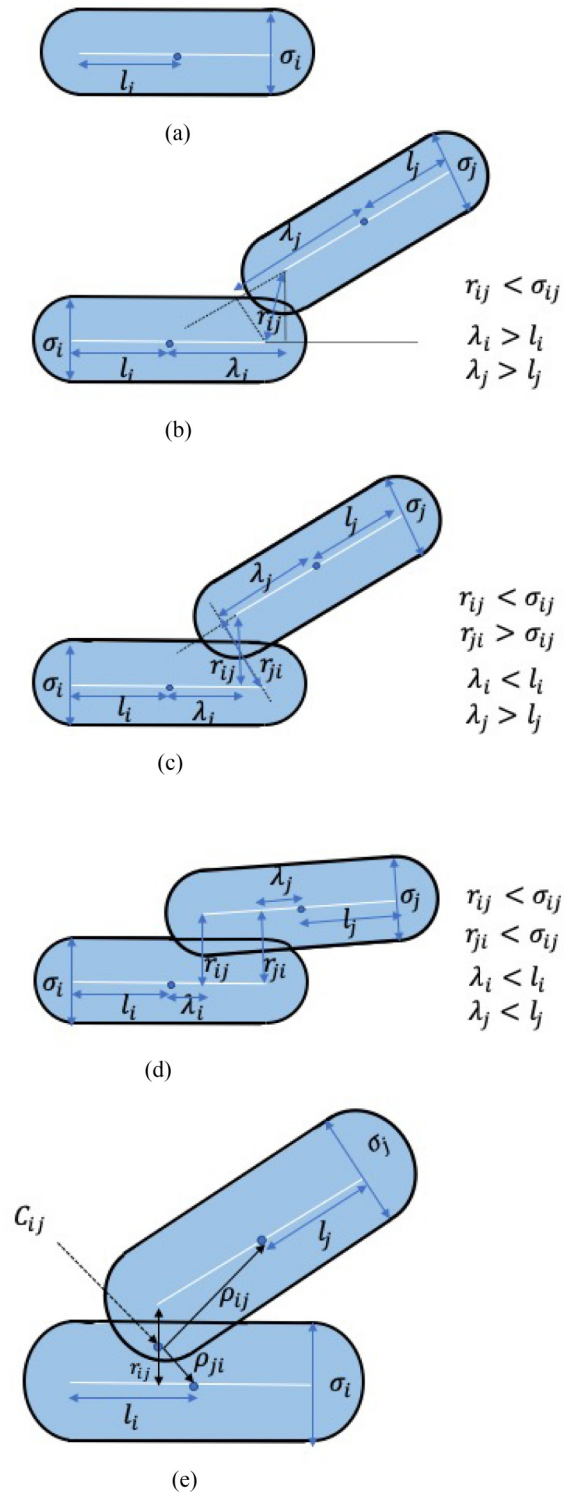


FIG. 1. (a) A single circulo-line with middle segment length $2l_i$ and end cap diameter σ_i . The three types of contacts between a pair of circulo-lines i and j : (b) an end-end contact, (c) an end-middle contact, and (d) a middle-middle contact. Note that $\sigma_{ij} = (\sigma_i + \sigma_j)/2$ and the distances r_{ij} , r_{ji} , λ_i , and λ_j are defined in the main text. (e) The effective point of contact C_{ij} between two overlapping circulo-lines i and j is located at the midpoint of r_{ij} . The vector $\bar{\rho}_{ij}$ points from C_{ij} to the center of circulo-line j . The overlaps between circulo-lines are magnified for visualization purposes; overlaps between particles are much less than 0.1% in the simulations.

Figure 1(d) shows two circulo-lines for which the two middle regions are in contact. We model middle-middle contacts as two end-middle contacts, so that when a middle-middle contact becomes an end-end contact [from Figs. 1(d) to 1(b)] or end-middle contact [from Figs. 1(d) to 1(c)] due to small changes in the positions and orientations of the circulo-lines, the interparticle potential energy and forces are continuous. Thus, for a middle-middle contact, the following four conditions must be satisfied: $r_{ij} < \sigma_{ij}$, $r_{ji} < \sigma_{ij}$, $\lambda_i < l_i$, and $\lambda_j < l_j$.

We seek to model elastic particles with purely repulsive interactions. Therefore, for all three types of contacts, we use the pairwise, purely repulsive, linear spring potential

$$U(r_{ij}) = \frac{\epsilon}{2} \left(1 - \frac{r_{ij}}{\sigma_{ij}}\right)^2 \Theta\left(1 - \frac{r_{ij}}{\sigma_{ij}}\right), \quad (1)$$

where ϵ is the characteristic energy scale of the interaction and $\Theta(\cdot)$ is the Heaviside step function, ensuring that pairs of circulo-lines do not interact when they are not in contact. We consider systems near jamming onset in the low-pressure limit, and thus the interparticle overlaps will be small. The contact rules in Fig. 1 ensure that the total potential energy, $U = \sum_{i>j} U(r_{ij})$, and pair forces, $\vec{f}_{ij} = (dU/dr_{ij})\hat{r}_{ij}$, are continuous as a function of the coordinates \vec{r}_i of the centers of mass and orientations θ_i of the circulo-lines. We use ϵ , ϵ/σ_s , and ϵ/σ_s^2 for the units of energy, force, and stress.

We employ the Love expression [32] to calculate the stress tensor:

$$\Sigma_{\alpha\beta} = \frac{1}{2L^2} \sum_{i,j=1}^N (f_{ij\alpha}\rho_{ij\beta} + f_{ij\beta}\rho_{ij\alpha}), \quad (2)$$

where $f_{ij\alpha}$ is the α component of the force on particle i due to particle j and $\rho_{ij\beta}$ is the β component of the vector pointing from the effective contact point between two overlapping circulo-lines i and j to the center of j . The effective contact point C_{ij} is the midpoint of r_{ij} as shown in Fig. 1(e). We define the pressure as $P = (\Sigma_{xx} + \Sigma_{yy})/2$ and the shear stress as $\Sigma = -\Sigma_{xy}$.

To calculate the shear modulus, we first apply an affine simple shear strain step $\delta\gamma$, which changes the circulo-line center of mass positions and orientations,

$$x'_i = x_i + \delta\gamma y_i, \quad (3)$$

and

$$\theta'_i = \cot^{-1}(\cot \theta_i + \delta\gamma), \quad (4)$$

together with Lees-Edwards shear-periodic boundary conditions, such that the two side walls tilt by $\delta\gamma$ relative to the horizontal axis [33]. (x_i, y_i) gives the position of the center of mass of the i th circulo-line and θ_i gives the angle that the axis of the circulo-line makes with the x axis. After each simple shear strain step, we minimize the total potential energy using the fast inertial relaxation engine (FIRE) algorithm [34] and measure the shear stress Σ . We can then determine the shear modulus by calculating $G = d\Sigma/d\gamma$.

We employ an athermal, quasistatic isotropic compression protocol to generate packings of circulo-lines at jamming onset. We initialize the system with random positions and orientations of the circulo-lines in the dilute limit with packing

fraction $\phi < 10^{-2}$. We then compress the system by $\Delta\phi/\phi = 2 \times 10^{-3}$ and minimize the total potential energy using the FIRE algorithm. We have verified that FIRE and the steepest descent energy minimization algorithms give the same value of the shear modulus for geometrical families of jammed disk and circulo-line packings as a function of pressure.

After energy minimization, we measure the pressure P and if $P < P_t$, where P_t is the target pressure, we again compress the system by $\Delta\phi$ and minimize the total potential energy. If $P > P_t$, we return to the previous configuration (before the most recent compression step) and decrease the packing fraction increment by a factor of 2. We continue this compression process until $|P - P_t|/P_t < 10^{-5}$. For $P_t < 10^{-7}$, we find that the number of interparticle contacts satisfies the effective isotropic condition: $N_c = N_c^0 - N_q$, where $N_c^0 = d_f N' - d + 1$, $d = 2$ is the spatial dimension, the number of degrees of freedom per particle is $d_f = 3$, $N' = N - N_r - N_s/3$, N_r is the number of rattler particles with too few contacts to constrain the d_f degrees of freedom per particle, and N_s is the number of slider particles with one unconstrained translational degree of freedom. For example, a circulo-line that is sandwiched between two other aligned circulo-lines (one on top and the other on the bottom) is a slider since it is free to move in the direction parallel to the neighboring particles. N_q is the number of quartic modes of the dynamical matrix [28]. For perturbations along quartic modes with amplitude δ , the change in potential energy scales as $\Delta U \sim \delta^4$, instead of $\Delta U \sim \delta^2$ for nonquartic modes. To investigate the pressure-dependent mechanical properties, we start with systems at $P_t = 10^{-7}$ and then successively increase the target pressure over the range $10^{-7} < P_t < 10^{-2}$.

III. RESULTS

Here, we describe our main results in five subsections. In Sec. III A, we generalize the concept of geometrical families of jammed packings in the ϕ - γ plane to packings of circulo-lines and show that the curvature $d^2\phi/d\gamma^2$ can be both positive and negative for packings of circulo-lines. In Sec. III B, we derive a general expression for the pressure-dependent shear modulus G in terms of derivatives of U and ϕ with respect to γ at fixed packing fraction and at fixed pressure. Using this expression, we find that the first geometrical family in the $P \rightarrow 0$ limit scales as $G_f/G_0 \sim 1 \pm P/P_0$ to linear order in P , where the sign of $d^2\phi/d\gamma^2$ determines the sign of the second term in G_f . In Sec. III C, we decompose the shear modulus for each low-pressure geometrical family, $G_f = G_a - G_{na}$, into the affine and nonaffine contributions, respectively. We show that the nonaffine contribution to the shear modulus of the low-pressure geometrical families is larger for packings of circulo-lines compared to that for disk packings, and that the pressure dependence of G_{na} can cause G_f to increase with pressure, which does not occur for packings of spherical particles. In Sec. III D, we characterize point and jump changes in the contact network during isotropic compression in packings of circulo-lines (interacting via repulsive linear springs) and show that jump changes give rise to discontinuous changes in potential energy, shear stress, and shear modulus, whereas point changes give rise to discontinuous changes only in the shear modulus. We find that

point changes are more frequent for packings of circulo-lines (compared to disk packings), but the resulting jumps in the shear modulus are smaller, over the same range of pressure as for disk packings. In Sec. III E, we discuss the results for the ensemble-averaged shear modulus $\langle G \rangle$ as a function of pressure. We show that, for large aspect ratios $\mathcal{R} \gtrsim 1.2$, $\langle G \rangle$ scales as a power-law at large pressures with an exponent that is nearly a factor of 2 larger than that for disk packings. For small aspect ratios, $\mathcal{R} \lesssim 1.2$, $\langle G \rangle$ versus pressure does not possess a single power-law scaling exponent. We further decompose $\langle G \rangle = \langle G_f \rangle + \langle G_r \rangle$ into contributions from geometrical families G_f and changes in the contact network G_r . We show that $\langle G_r \rangle$ is smaller for packings of circulo-lines compared to that for spherical particles, and thus the increase in the power-law exponent is caused by the fact that the shear modulus can increase in pressure during geometrical families for packings of circulo-lines.

A. Geometrical families of circulo-lines

Jammed packings within a geometrical family are mechanically stable packings with different values of the pressure (and shear stress) that are related to each other by continuous, quasistatic changes in packing fraction and shear strain with no changes in the interparticle contact network. We showed in previous studies of jammed disk packings that near-isostatic geometrical families form upward parabolic segments in the ϕ - γ plane [31,35]. An example geometrical family of $N = 6$ jammed disk packings in the $P \rightarrow 0$ limit runs from point A to point B in Fig. 2(a). Similarly shaped geometrical families occur at higher pressures, as shown by the upward parabolic contours in Fig. 2(a). We show the pressure versus the total potential energy U and shear strain γ in Fig. 2(b) for the same data in Fig. 2(a).

Geometrical families begin and end at point or jump changes in the interparticle contact network [22]. For example, after making an infinitesimal increase in shear strain at point C ($\gamma \sim 0.50$) in Fig. 2(a), the system undergoes a jump change to point D. At a jump change, the packing becomes unstable, particles rearrange, and the packing fraction, shear stress, and shear modulus change discontinuously. At point B ($\gamma \sim 0.49$) in Fig. 2(a), the system undergoes a point change. For point changes, a single contact is added or removed from the contact network and the packing fraction and shear stress are continuous. For packings with purely repulsive linear spring interactions, the shear modulus is discontinuous at point changes [22].

In Fig. 3(a), we show the structure of geometrical families in the ϕ - γ plane for jammed packings of $N = 6$ bidisperse circulo-lines with aspect ratio $\mathcal{R} = 2.0$. As for jammed disk packings, we find that packings of circulo-lines can form upward parabolic geometrical families, e.g., from point (b) to (c) in Fig. 3(a). The configurations that correspond to the beginning and end of this geometrical family are shown in Figs. 3(b) and 3(c). These two configurations share the same contact network, but the relative angles that the circulo-lines make with each other are different; e.g., circulo-lines 3 and 4 in Fig. 3(c) are tilted away from the horizontal axis compared to those in Fig. 3(b).

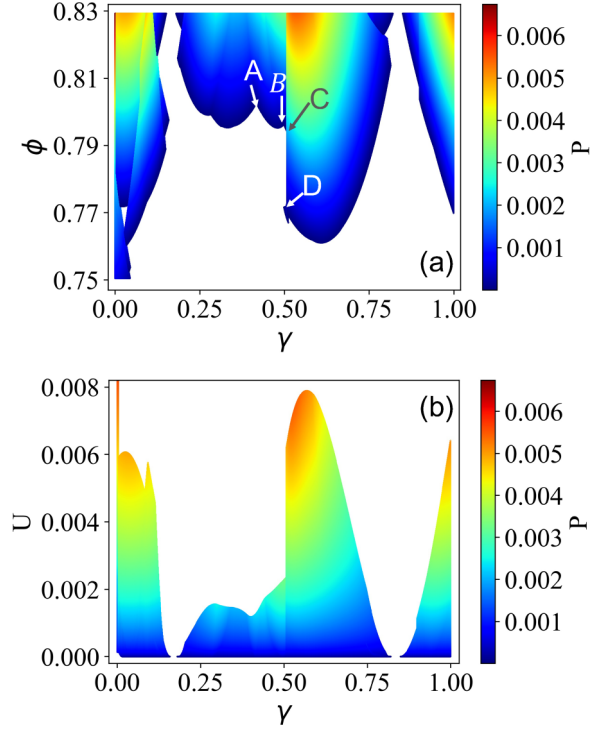


FIG. 2. (a) Pressure P for jammed packings of $N = 6$ bidisperse disks as a function of packing fraction ϕ and shear strain γ . White regions correspond to unjammed states. Points A and B correspond to the beginning and end of a geometrical family in the $P \rightarrow 0$ limit. At point B ($\gamma \sim 0.49$), the system undergoes a point change to the next geometrical family that ends at point C. At point C ($\gamma \sim 0.50$), the system undergoes a jump change to the next geometrical family that starts at point D. (b) The same data as in (a), except we show P as a function of the total potential energy U and γ .

Because pairs of circulo-lines can form three different types of contacts, the contact network can change when particles i and j form or break a contact, as well as when the type of contact between i and j changes (e.g., from an end-end to an end-middle contact). (See Sec. II). As a result, packings of circulo-lines possess more point changes and shorter geometrical families in the ϕ - γ plane than disk packings. For example, the average terminus P_{end} of the lowest-pressure geometrical family is a factor of 5 larger for $N = 6$ disk packings compared to $N = 6$ packings of circulo-lines with $\mathcal{R} = 2$. In response to an infinitesimal increase in shear strain at point (c) in Fig. 3(a), the system undergoes a jump change to point (d). There are a total of eight changes in the contact network across the jump change, e.g., circulo-lines 1 and 2 are in contact in Fig. 3(c), but they are not in contact in Fig. 3(d) and the types of contacts between circulo-lines 3 and 4 change between Figs. 3(c) and 3(d) (from end-middle to middle-end or from middle-end to end-middle). At a jump change in packings of circulo-lines, the packing fraction, shear stress, and shear modulus also change discontinuously. (See Sec. III D below).

Another upward geometrical family occurs between points (d) and (e) in Fig. 3(a). At point (e), the system undergoes a point change. As shown in Figs. 3(e) and 3(f), the system loses a single contact across the point change. The packing fraction and shear stress are continuous, whereas we will show

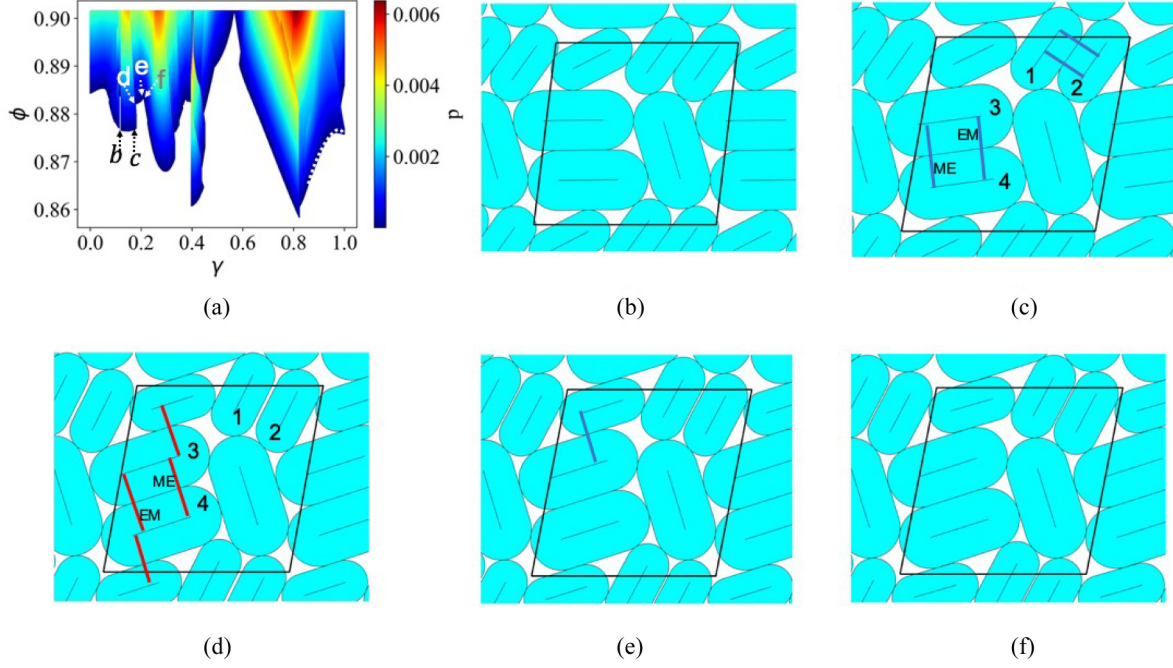


FIG. 3. (a) Pressure P for jammed packings of $N = 6$ bidisperse circulo-lines with aspect ratio $\mathcal{R} = 2.0$ as a function of packing fraction ϕ and shear strain γ . White regions correspond to unjammed states. Points (b) and (c) correspond to the beginning and end of an upward geometrical family. At point (c) ($\gamma \sim 0.19$), the system undergoes a jump change to point (d). A second upward geometrical family occurs between points (d) and (e). The system undergoes a point change from points (e) to (f) ($\gamma \sim 0.205$). We also show a downward geometrical family in the $P \rightarrow 0$ limit (dotted line) that extends from $\gamma \sim 0.82$ to 1. The packings in (b)–(f) correspond to points (b)–(f) in the ϕ - γ plane in (a). The highlighted contacts in (c) do not occur in (d), and the highlighted contacts in (d) do not occur in (c). The highlighted contact in (e) does not occur in (f). EM (or ME) indicates an end-middle (or middle-end) contact between circulo-lines 3 and 4.

in Sec. III D that the shear modulus is discontinuous across a point change (for purely repulsive, linear spring interactions).

In contrast to jammed disk packings, the geometrical families for packings of circulo-lines can form both upward and downward parabolic segments in the ϕ - γ plane. One of the downward geometrical families is highlighted from $\gamma \sim 0.82$ to 1 in Fig. 3(a). In the next section, we show that the sign of the curvature of the parabolic geometrical families determines whether the shear modulus of the geometrical family increases or decreases with pressure.

B. Stress-dilatancy relation

We now derive an exact expression for the shear modulus in terms of derivatives of the total potential energy U , packing fraction ϕ , and pressure P with respect to the shear strain γ . This expression will enable us to understand the behavior of $G(P)$ within geometrical families. If we take infinitesimal steps $d\phi$ and $d\gamma$ along a geometrical family in the ϕ - γ plane, the change in the total potential energy is

$$dU = -PdA - \Sigma_{xy}Ad\gamma, \quad (5)$$

where $A = L^2$ is the area of the system and $dA/A = -d\phi/\phi$. After rearranging Eq. (5), we find the following expression that relates the shear stress to the dilatancy $-\phi^{-1}(d\phi/d\gamma)_P$ at finite pressure [31]:

$$\Sigma = \frac{1}{L^2} \left(\frac{dU}{d\gamma} \right)_P - \frac{P}{\phi} \left(\frac{d\phi}{d\gamma} \right)_P. \quad (6)$$

The shear modulus can be obtained by calculating the derivative $d\Sigma/d\gamma$ at constant packing fraction:

$$G = \left(\frac{d\Sigma}{d\gamma} \right)_\phi = \frac{1}{L^2} \left(\frac{d \left(\frac{dU}{d\gamma} \right)_P}{d\gamma} \right)_\phi - \frac{P}{\phi} \left(\frac{d \left(\frac{d\phi}{d\gamma} \right)_P}{d\gamma} \right)_\phi - \frac{1}{\phi} \left(\frac{dP}{d\gamma} \right)_\phi \left(\frac{d\phi}{d\gamma} \right)_P. \quad (7)$$

The shear modulus is a sum of three terms, $G = G_1 + G_2 + G_3$, where $G_1 = L^{-2}(d(dU/d\gamma)_P/d\gamma)_\phi$ includes mixed derivatives of U with respect to γ at fixed ϕ and at fixed P , $G_2 = -P\phi^{-1}(d(d\phi/d\gamma)_P/d\gamma)_\phi$ is proportional to the derivative of the dilatancy with respect to γ at fixed ϕ , and $G_3 = -\phi^{-1}(dP/d\gamma)_\phi(d\phi/d\gamma)_P$ includes shear strain derivatives of P at fixed ϕ and of ϕ at fixed P . Since $\phi(\gamma)$ is approximately parabolic at low pressures, G_2 is proportional to pressure and G_3 is nonzero in the $P \rightarrow 0$ limit. In contrast, G_1 involves two derivatives of the total potential energy U with respect to shear strain γ . In Fig. 2(b), we show that (for the regions of shear strain where jammed packings exist) the potential energy U does not vary strongly with γ at low pressures. Thus, we expect that $|G_1|$ is small in the low-pressure regime, and instead variations of $\phi(\gamma)$ determine the mechanical properties of the system.

Equation (7) is verified numerically for a low-pressure geometrical family of circulo-line packings for which G increases with P in Fig. 4(a). For all disk and circulo-line packings that

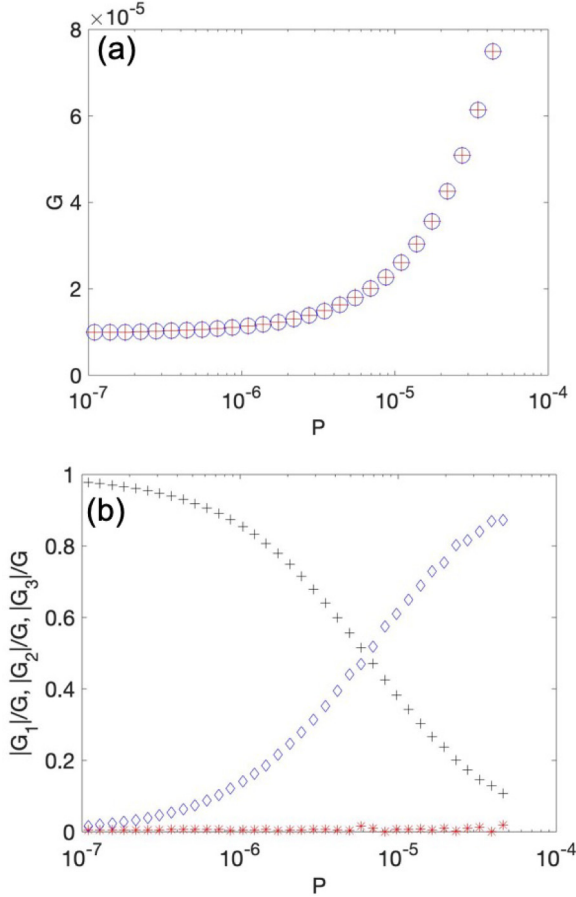


FIG. 4. (a) Comparison of the shear modulus G versus pressure P for $N = 16$ jammed packings of bidisperse circulo-lines with $\mathcal{R} = 2$ obtained by calculating $G = d\Sigma/d\gamma$ numerically (circles) and by calculating the three terms $G = G_1 + G_2 + G_3$ in Eq. (7) individually (crosses). Note that G increases with P for this geometrical family. (b) $|G_1|/G$ (asterisks), $|G_2|/G$ (diamonds), and $|G_3|/G$ (crosses) as defined in Eq. (7) for the same data in (a).

we have considered, $|G_1| \ll |G_2|$ or $|G_1| \ll |G_3|$, and thus the first term G_1 in Eq. (7) can be neglected. Furthermore, we show in Fig. 4(b) for an $N = 16$ packing of circulo-lines with $\mathcal{R} = 2$ that $|G_3| > |G_2|$ for $P < P'$ and $|G_2| > |G_3|$ for $P > P'$. ($P' \sim 10^{-5}$ for this particular system size and aspect ratio). We find that $G \sim G_3 \sim G_0 > 0$ in the zero-pressure limit, and thus the shear modulus for low-pressure geometrical families can be approximated as $G \sim G_0 + \eta P$, where η is determined by the negative curvature of the geometrical families in the ϕ - γ plane. In particular, $\eta > 0$ ($\eta < 0$) for downward (upward) geometrical families in the ϕ - γ plane. In Fig. 5, we show the shear modulus versus pressure for 50 low-pressure geometrical families of $N = 16$ bidisperse packings of circulo-lines with $\mathcal{R} = 2$. We show that the shear modulus obeys $G \sim G_0 + \eta P$ within each geometrical family. For this system size and aspect ratio, approximately half of the geometrical families have $\eta > 0$ and the other half have $\eta < 0$. The fact that a finite fraction of geometrical families possesses upward geometrical families with $\eta > 0$ strongly influences the ensemble-averaged shear modulus $\langle G \rangle$ as discussed in Sec. III E.

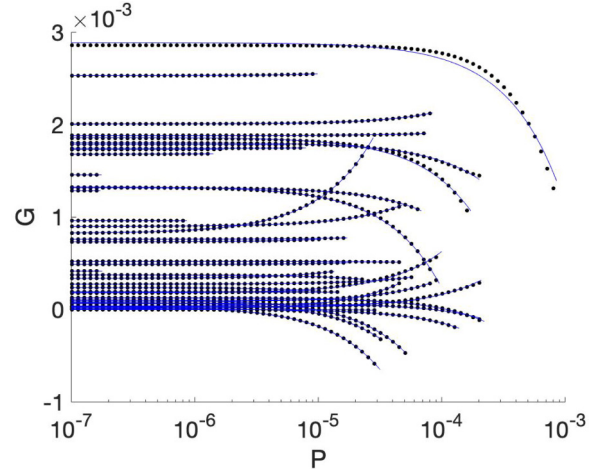


FIG. 5. The shear modulus G versus the pressure P for $N = 16$ jammed packings of bidisperse circulo-lines with aspect ratio $\mathcal{R} = 2.0$. We show 50 different low-pressure geometrical families (black circles) and each geometrical family ends at a point or jump change in the interparticle contact network. The blue solid lines are best fits to $G = G_0 + \eta P$.

C. Affine and nonaffine contributions to the shear modulus for geometrical families

The shear modulus can be decomposed into the affine and nonaffine contributions: $G = G_a - G_{na}$, where the affine contribution, $G_a = L^{-2}d^2U/d\gamma^2$, is obtained by applying a global, affine simple shear strain and the nonaffine contribution, G_{na} , includes the relaxation process during potential energy minimization following the applied affine shear strain. Explicit expressions for the affine contribution for circulo-line packings are provided in the Appendix. Numerous prior studies have shown that the nonaffine response dominates the shear modulus in disk packings near jamming onset [36–40]. Similar calculations of the nonaffine contribution to the shear modulus of jammed packings of nonspherical particles have not been performed.

In previous studies [24], we calculated $G_{na} = G - G_a$ for isostatic geometrical families of jammed disk packings. These results are also shown in Fig. 6(a) for $N = 16$ disk packings. We find that G_{na} increases with pressure, which causes jammed disk packings to soften (i.e., G decreases) along compression geometrical families. If changes in the contact network do not occur until relatively large pressures, the packings can be strained toward a mechanical instability, where the nonaffine particle motion and nonaffine contribution to the shear modulus increase dramatically, causing deviations from the simple form $G_{na} \sim G'_0 + \eta'P$, and the total shear modulus $G = G_a - G_{na}$ decreases more strongly than linearly with pressure. In contrast, when a geometrical family ends (via a change in the contact network) at a relatively small pressure, G_{na} for disk packings increases linearly with pressure and the total shear modulus decreases linearly with pressure.

We now describe similar studies of G_{na} for low-pressure geometrical families of circulo-lines, as shown in Fig. 6(b) for $\mathcal{R} = 2.0$. We identify several results concerning G_{na} for packings of circulo-lines that are different from the results for disk packings. First, as discussed above, the average pressure

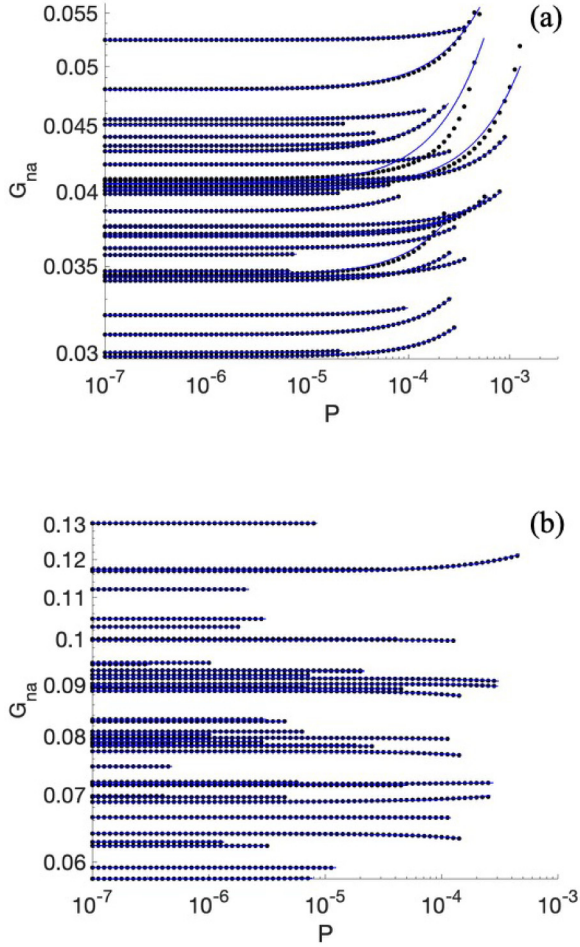


FIG. 6. (a) The nonaffine contribution to the shear modulus G_{na} versus pressure P for 30 low-pressure geometrical families of $N = 16$ jammed disk packings (black dots). (b) G_{na} versus P for 57 low-pressure geometrical families of $N = 16$ bidisperse circulo-line packings with $\mathcal{R} = 2.0$ (black dots). Each geometrical family ends at a point or jump change in the interparticle contact network. The solid blue lines in both panels are fits to $G_{na} \sim G'_0 + \eta'P$.

range over which the first, low-pressure geometrical families persist is smaller for packings of circulo-lines, and $G_{na}(P)$ is well fit by $G_{na}(P) \sim G'_0 + \eta'P$. Second, G_{na} can either increase or decrease with pressure (i.e., $\eta' > 0$ or $\eta' < 0$). In particular, packings of circulo-lines can harden (i.e., G increases) along compression geometrical families, in contrast to disk packings. In addition, the ensemble-averaged $\langle G_{na} \rangle$ for the first geometrical family is typically larger for packings of circulo-lines compared to that for disk packings. For example, for packings of circulo-lines with $\mathcal{R} = 2.0$, $\langle G_{na} \rangle$ is more than a factor of 2 larger than $\langle G_{na} \rangle$ for disk packings.

D. Point and jump changes in the contact network

In previous studies [22] of jammed packings of disks that interact via purely repulsive, linear spring potentials, we found that the shear modulus possesses discontinuous jumps when the packings undergo point and jump changes in the interparticle contact networks during applied deformations (such as shear or compression). Point changes are additions or

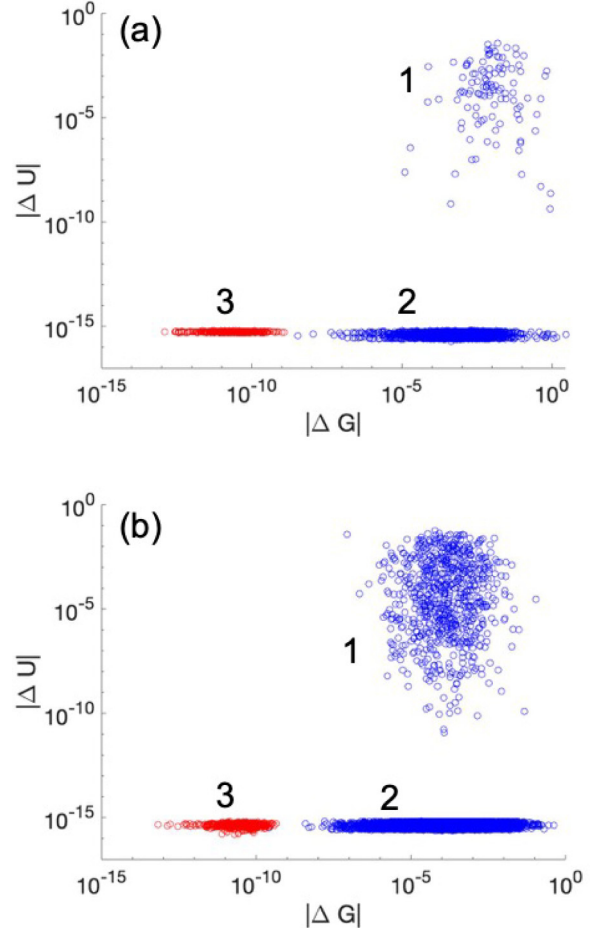


FIG. 7. (a) Scatter plot of the change in the shear modulus $|\Delta G|$ versus the change in the potential energy $|\Delta U|$ measured between packings separated by small compression steps for $N = 128$ disk packings. (b) Same data as in (a), but for $N = 128$ circulo-line packings with $\mathcal{R} = 2.0$. The red dots in region 3 indicate comparisons between two packings with the same interparticle contact networks. The blue points in regions 1 and 2 correspond to jump and point changes, respectively.

removals of a single contact in the network. In contrast, jump changes are caused by mechanical instabilities and involve multiple contact changes and significant particle motion. In Fig. 7(a), we show a scatter plot of changes in G and the potential energy U between jammed $N = 128$ disk packings that are separated by small compression steps over a range of pressure $10^{-3} < P < 10^{-2}$. To generate Fig. 7(a), we identify the pressures at the beginning and end of all geometrical families in this pressure range ($10^{-3} < P < 10^{-2}$) and compare G and U between two packings before the contact network change and one before and one after the contact network change.

We identify three regions of clustered points in Fig. 7(a): regions with (1) large $|\Delta G|$ and large $|\Delta U|$, (2) large $|\Delta G|$ and small $|\Delta U|$, or (3) small $|\Delta G|$ and small $|\Delta U|$. The interparticle contact networks change for the systems in regions 1 and 2, and data in these regions correspond to jump and point changes, respectively. For the data in region 3, the contact

network does not change, and $|\Delta G|$ and $|\Delta U|$ will decrease with improved force balance.

In Fig. 7(b), we show similar data for $|\Delta G|$ and $|\Delta U|$ for $N = 128$ jammed packings of circulo-lines with $\mathcal{R} = 2.0$ over the same pressure range as studied for jammed disk packings. As found previously for disk packings, jammed packings of circulo-lines undergo point and jump changes in the contact network, which lead to discontinuous jumps in G . As found previously, point and jump changes can be differentiated because point changes have vanishing $|\Delta U|$, whereas jump changes have nonzero values of $|\Delta U|$.

For the jammed disk packings considered in Fig. 7(a), jump changes accounted for ~ 0.13 of the changes in the contact network. However, jump changes accounted for only ~ 0.03 of the changes in the contact network for jammed circulo-line packings over the same range of pressure. Since point changes can involve changes in the *type* of contact between the same pair of particles, point changes are much more frequent in packings of circulo-lines compared to disk packings.

E. Ensemble-averaged shear modulus

Numerous prior studies have shown that the ensemble-averaged shear modulus $\langle G \rangle$ for packings of frictionless, spherical particles increases as a power law in pressure when $P > P^{**}$ [12,17], where $P^{**} \sim N^{-2}$ decreases with increasing system size. For finite-sized systems, we have used the following scaling form for the ensemble-averaged shear modulus [21]:

$$\langle G \rangle = \langle G_0 \rangle + \frac{bP^\chi}{1 + cP^{\chi-\beta}}, \quad (8)$$

where $\langle G_0 \rangle \sim N^{-1}$, b and c are constants, χ and β are power-law exponents, and the large-pressure scaling exponent $\beta \sim 0.5$ for packings of spherical particles with repulsive linear spring interactions. [See Fig. 8(a)].

In Fig. 8(b), we show $\langle G \rangle$ versus P for packings of circulo-lines with $\mathcal{R} = 1.5$ for several system sizes. As for disk packings, $\langle G \rangle = \langle G_0 \rangle \sim N^{-1}$ in the zero-pressure limit and $\langle G(P) \rangle$ increases as a power law at large pressure. For packings of circulo-lines with $\mathcal{R} \gtrsim 1.2$, we find that a scaling function with a single power law [i.e., $c = 0$ in Eq. (8)] provides a better description of $\langle G \rangle$ versus P over the full range of pressure. We find that the power-law exponent $\chi \sim 0.9$ for $\mathcal{R} = 1.5$, suggesting that the pressure-dependent mechanical properties of jammed packings of circulo-lines differ from those of jammed disk packings.

In Fig. 9, we show $\langle G \rangle$ (normalized by the zero-pressure value $\langle G_0 \rangle$) versus P over a range of aspect ratios (for a single system size $N = 128$). In Fig. 9(a), we compare $\langle G \rangle / \langle G_0 \rangle$ for packings of circulo-lines with large aspect ratios ($\mathcal{R} = 1.5$ and 2) and for disk packings. $\langle G \rangle / \langle G_0 \rangle$ for the packings with large aspect ratios has a robust large-pressure scaling exponent χ that is larger than that for disk packings. The inset to Fig. 8(b) shows that $0.8 \lesssim \chi \lesssim 0.9$ for $\mathcal{R} > 1.2$. In Fig. 9(b), we show $\langle G \rangle / \langle G_0 \rangle$ versus P for small aspect ratios $\mathcal{R} \leq 1.2$. $\langle G \rangle / \langle G_0 \rangle$ no longer has a single large-pressure scaling exponent. The curves have a steep region in the intermediate pressure regime from 10^{-5} to $10^{-3.5}$, with scaling exponents that are comparable to those for higher aspect ratios. However,

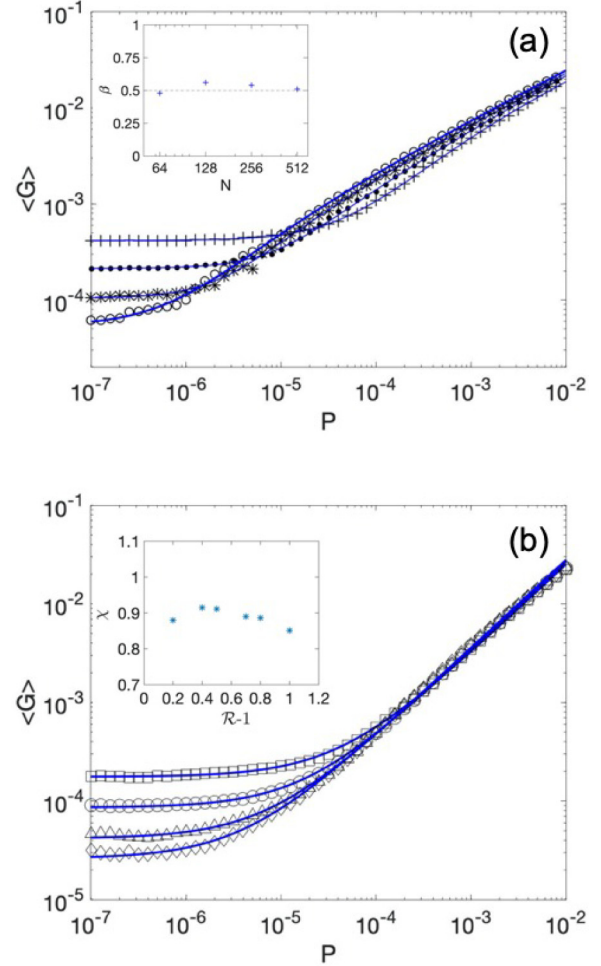


FIG. 8. (a) Ensemble-averaged shear modulus $\langle G \rangle$ versus pressure P for bidisperse disk packings for several system sizes: $N = 64$ (crosses), 128 (solid circles), 256 (asterisks), and 512 (open circles). The solid lines are best fits to Eq. (8). The inset shows the large-pressure power-law scaling exponent β versus N . (b) Similar data as in (a), but for packings of circulo-lines with $\mathcal{R} = 1.5$ and $N = 64$ (squares), 128 (circles), 256 (triangles), and 512 (diamonds). The solid lines are best fits to Eq. (8) with $c = 0$. The inset shows the large-pressure scaling exponent χ versus $\mathcal{R} - 1$. In both panels, the averages are calculated over 10^3 different initial conditions.

at larger pressures above a characteristic pressure, $P > P^*$, the curves bend over and have scaling exponents that are much less than those in the inset to Fig. 8(b). The data also suggest that P^* decreases as the aspect ratio decreases, indicating that the range of pressure over which the elevated scaling exponent occurs decreases as $\mathcal{R} \rightarrow 1$.

To explain the increase in the power-law scaling exponent for packings of circulo-lines, we decompose the ensemble-averaged shear modulus $\langle G \rangle$ into contributions from geometrical families, $\langle G_f \rangle$, and from discontinuous jumps caused by changes in the interparticle contact network, $\langle G_r \rangle$: $\langle G \rangle = \langle G_f \rangle + \langle G_r \rangle$ [21,24]. In Fig. 10(a), we compare $\langle G_f \rangle / \langle G_0 \rangle$ and $\langle G_r \rangle / \langle G_0 \rangle$ for packings of circulo-lines with $\mathcal{R} = 1.5$ and for disk packings both with $N = 128$. For jammed disk packings, $\langle G_f \rangle / \langle G_0 \rangle$ decreases monotonically with increasing pressure, and thus there is a characteristic

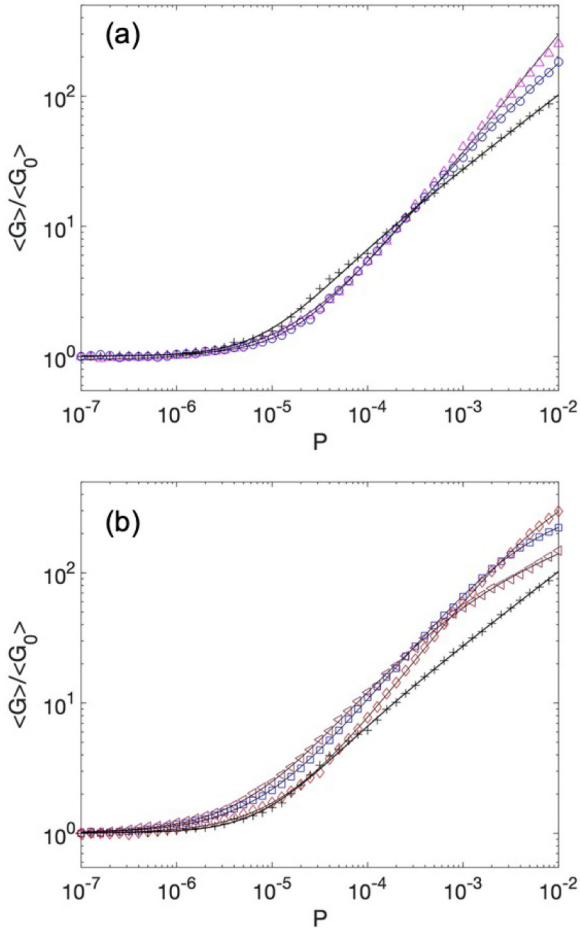


FIG. 9. (a) Ensemble-averaged shear modulus $\langle G \rangle$ (normalized by the zero-pressure value $\langle G_0 \rangle$) versus pressure P for $N = 128$ packings of circulo-lines with several aspect ratios: $\mathcal{R} = 1$ (crosses), 1.5 (upward triangles), and 2 (circles). (b) Similar data as in (a), except for $\mathcal{R} = 1$ (crosses), 1.05 (leftward triangles), 1.1 (squares), and 1.2 (diamonds). In both panels, the solid lines are fits to Eq. (8). For $\mathcal{R} > 1.2$, $c = 0$. $\langle G \rangle$ is calculated using 10^3 different initial conditions.

pressure $\langle P_0 \rangle$ at which $\langle G_f \rangle = 0$ and above which $\langle G_f \rangle < 0$. For $N = 128$ jammed disk packings, $\langle P_0 \rangle \sim 10^{-5}$. Thus, for $P > \langle P_0 \rangle$, the difference between the rearrangement and geometrical family contributions, $\langle G \rangle = \langle G_r \rangle - |\langle G_f \rangle|$, determines the power-law scaling behavior of the shear modulus with pressure for jammed disk packings.

A key difference between jammed disk packings and packings of circulo-lines is that circulo-line packings possess a finite fraction of geometrical families whose shear modulus increases with pressure [see inset of Fig. 10(a)], which can cause $\langle G_f \rangle / \langle G_0 \rangle$ to increase with pressure. For $\mathcal{R} = 1.5$ circulo-line packings with $N = 128$, we find that $\langle G_f \rangle / \langle G_0 \rangle$ increases over a wide pressure range $10^{-7} \lesssim P \lesssim 10^{-3.5}$. For $P \gtrsim 10^{-3.5}$, the fraction of geometrical families that increases with pressure, p_{up} , decreases dramatically, and $\langle G_f \rangle / \langle G_0 \rangle$ begins decreasing with pressure. $\langle G_f \rangle / \langle G_0 \rangle$ reaches zero near $\langle P_0 \rangle \sim 10^{-2.5}$ and continues decreasing with further increases in pressure.

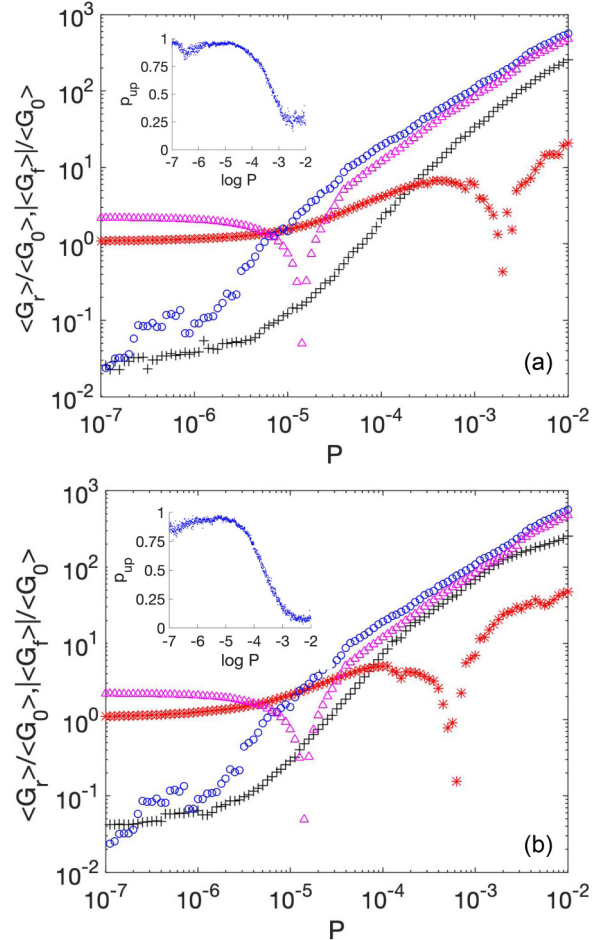


FIG. 10. The average rearrangement $\langle G_r \rangle$ (crosses) and geometrical family $|\langle G_f \rangle|$ (asterisks) contributions to the shear modulus for $N = 128$ jammed packings of circulo-lines (normalized by the average zero-pressure value of the shear modulus, $\langle G_0 \rangle$) for (a) $\mathcal{R} = 1.5$ and (b) 1.1. As a comparison, we also show $\langle G_r \rangle$ (circles) and $|\langle G_f \rangle|$ (triangles) for $N = 128$ disk packings. In each panel, the inset shows the probability p_{up} that each geometrical family increases with pressure, obtained from 500 jammed packings of circulo-lines at each small pressure interval.

In addition, the rearrangement contribution $\langle G_r \rangle / \langle G_0 \rangle$ is larger for disk packings compared to packings of circulo-lines with $\mathcal{R} = 1.5$, as shown in Fig. 10(a). Thus, even though the frequency of contact network changes is enhanced for packings of circulo-lines (see Sec. III D), the discontinuous jumps in the shear modulus are sufficiently small for circulo-line packings that $\langle G_r \rangle / \langle G_0 \rangle$ is larger for disk packings. Since $\langle G_r \rangle / \langle G_0 \rangle$ is larger for jammed disk packings compared to circulo-line packings and $\langle G_f \rangle / \langle G_0 \rangle$ increases with pressure over a wide range of pressure, it is clear that the existence of geometrical families with shear moduli that increase with pressure is responsible for the elevated power-law scaling exponent for packings of circulo-lines with $\mathcal{R} \gtrsim 1.2$.

For jammed packings of circulo-lines with $\mathcal{R} \lesssim 1.2$, we do not find a single power-law scaling exponent for $\langle G \rangle$ versus P . Instead, $\langle G(P) \rangle$ has a power-law exponent $\beta \sim 0.8\text{--}0.9$ for intermediate pressures and then the exponent decreases for $P \gtrsim 10^{-2.5}$. [See Fig. 9(b)]. In Fig. 10(b), we show that $\langle G_r \rangle$ is

much larger for circulo-line packings with $\mathcal{R} = 1.1$ than that with 1.5. In particular, $\langle G_r \rangle$ for $\mathcal{R} = 1.1$ is comparable to that for jammed disk packings for $P \gtrsim 10^{-4}$ and $\langle G_f \rangle > 0$ over a much narrower range of pressure. The two results cause the lack of single power-law scaling for packings of circulo-lines with $\mathcal{R} \lesssim 1.2$.

IV. CONCLUSIONS AND FUTURE DIRECTIONS

In this article, we studied the structural and mechanical properties of jammed packings of circulo-lines with frictionless, purely repulsive, linear spring interactions. We found several important results for jammed packings of circulo-lines that are different from those for jammed packings of spherical particles. First, we showed that packings of circulo-lines possess geometrical families that can be both concave upward or concave downward in the packing fraction-shear strain (ϕ - γ) plane. In contrast, the geometrical families are nearly always concave upward in the ϕ - γ plane, especially at low pressure, for jammed packings of spherical particles. We then derived a stress-dilatancy relation for packings at finite pressure, which allowed us to show that the shear modulus for low-pressure geometrical families obeys $G_f = G_0 + \eta P$ to linear order in pressure, where the sign of η is determined by the negative curvature of geometrical families in the ϕ - γ plane. Thus, the shear modulus of low-pressure geometrical families increases with pressure when $d^2\phi/d\gamma^2 < 0$ and decreases with pressure when $d^2\phi/d\gamma^2 > 0$. The fact that the shear modulus of geometrical families can increase with pressure has a profound effect on the pressure-dependent, ensemble-averaged shear modulus $\langle G(P) \rangle$. In particular, we found that $\langle G(P) \rangle$ for jammed packings of circulo-lines with aspect ratios $\mathcal{R} \gtrsim 1.2$ displays robust power-law scaling over a wide range of pressure, but the scaling exponent ($\beta \sim 0.8$ – 0.9) is nearly a factor of 2 larger than that for jammed disk packings ($\beta \sim 0.5$). For smaller aspect ratios, $\mathcal{R} \lesssim 1.2$, $\langle G(P) \rangle$ does not possess a single power-law scaling exponent over the same range of pressure. To understand the origin of this behavior, we decomposed $\langle G \rangle$ into separate contributions from geometrical families, $\langle G_f \rangle$, and from changes in the contact network, $\langle G_r \rangle$: $\langle G \rangle / \langle G_0 \rangle = \langle G_f \rangle / \langle G_0 \rangle + \langle G_r \rangle / \langle G_0 \rangle$, where $\langle G_0 \rangle$ is the value of $\langle G \rangle$ in the zero-pressure limit. In general, we found that $\langle G_r \rangle / \langle G_0 \rangle$ is larger for disk packings compared to that for packings of circulo-lines, even though the frequency of changes in the contact network is larger for packings of circulo-lines. In contrast, we found that $\langle G_f \rangle / \langle G_0 \rangle$ is much larger for packings of circulo-lines. In fact, $\langle G_f \rangle / \langle G_0 \rangle < 0$ for disk packings, whereas it can be positive for packings of circulo-lines in the pressure regime where the power-law scaling exponent is larger than that for disk packings. Thus, the presence of geometrical families with shear moduli that increase with pressure gives rise to important changes in the pressure-dependent mechanical properties for jammed packings of circulo-lines.

These results suggest several promising areas of future research. First, in the present studies, we did not examine in detail how properties of jammed packings of circulo-lines in the $\mathcal{R} \rightarrow 1$ limit compare to those for jammed disk packings. Two issues arise in the $\mathcal{R} \rightarrow 1$ limit:

(1) Noncircular particles always possess three degrees of freedom per particle, whereas smooth disks possess only two nontrivial degrees of freedom per particle. Thus, in future studies, we will compare the properties of jammed packings of circulo-lines to those for packings of weakly frictional or bumpy particles, which both possess three degrees of freedom per particle [41].

(2) The current force model for circulo-lines, which considers forces between the end and middle sections of pairs of circulo-lines, does not converge to the force model obtained from Eq. (1) in the $\mathcal{R} \rightarrow 1$ limit for packings with finite pressure. A force law that is a function of the square root of the area of overlap between pairs of circulo-lines is a more promising model.

Another promising area of future research involves studies of how the mechanical response of jammed packings depends on both the particle shape and form of the interparticle potential. In previous studies of jammed disk packings [24], we found that the shear modulus G of near-isostatic geometric families scales with pressure P as $G \sim (P/P_0)^{(\alpha-2)/(\alpha-1)} - P/P_0$, where P_0 is the pressure at which $G = 0$ and $\alpha = 2, 5/2$ for repulsive linear and Hertzian spring potentials, respectively. Based on the results found here, we predict that the shear modulus for near-isostatic geometrical families of circulo-lines with repulsive Hertzian spring interactions will scale as $G \sim (P/P_0)^{1/3} \pm P/P_0$, where the sign of the second term depends on whether the geometrical family is concave downward or upward in the packing fraction and shear strain plane. Thus, the scaling of the ensemble-averaged shear modulus versus pressure for jammed packings of circulo-lines with repulsive Hertzian spring interactions will differ from the current results. However, there is currently no theoretical framework that can predict $\langle G(P) \rangle$ based on the statistics and pressure dependence of the shear moduli of geometrical families.

Third, we know that jammed packings of circulo-lines possess concave upward and concave downward geometrical families in the ϕ - γ plane. Do jammed packings of other nonspherical particle shapes also possess concave upward and concave downward geometrical families? Can we find particle shapes for which jammed packings only possess concave downward geometrical families in the ϕ - γ plane? We have shown in previous studies that the power-law scaling exponent for $\langle G(P) \rangle$ for jammed packings of ellipse-shaped particles is also elevated relative to that for jammed disk packings [25,26]. Thus, it is likely that jammed packings of ellipse-shaped particles also possess concave downward geometrical families in the ϕ - γ plane. Since the power-law scaling exponent β for $\langle G(P) \rangle$ depends on properties of the geometrical families, the frequency of contact network changes, and the size of the discontinuous jumps in G caused by the contact network changes, it seems likely that the power-law scaling exponent β will depend sensitively on particle shape. Thus, it will be important to study $\langle G(P) \rangle$ and other mechanical properties for packings of different particle shapes in both two and three dimensions. The results from these studies will allow us to develop a theoretical framework that can predict the power-law scaling behavior of $\langle G(P) \rangle$ in terms of the statistics of changes in the interparticle contact network and the form of the shear modulus of geometrical families.

In addition, we have shown that the shear modulus can become negative in jammed packings when they are sheared using strain control [24]. For example, for jammed disk packings with repulsive linear spring interactions, the shear modulus for near-isostatic geometrical families scales as $G/G_0 \sim 1 - P/P_0$ at low pressure, where G_0 is a constant and P_0 is the pressure at which G becomes zero. Thus, as the pressure increases from zero, and if there are no changes in the interparticle contact network, the shear modulus of geometrical families can decrease to zero and, with further increases in pressure, become negative. For the isotropic compression protocol that we employ, the number of geometrical families with negative shear moduli is sufficiently large that the ensemble average is affected. The ensemble-averaged shear modulus for geometrical families $|\langle G_f \rangle|$ in Fig. 10, which is plotted on a logarithmic scale versus pressure, displays a deep cusp at a characteristic pressure where $|\langle G_f \rangle|$ approaches zero. The shear modulus of individual geometrical families can become negative over a wide range of pressures, but there are not enough of these to cause the ensemble average to vanish at other values of the pressure. An important topic for future research is to understand whether different protocols for generating jammed packings [35] in the ϕ - γ plane (such as varying the rate at which energy is removed from the system) can affect the frequency and range of pressure over which geometrical families possess negative shear moduli. If so, different packing-generation protocols can give rise to different behavior for the ensemble-averaged shear modulus, $\langle G(P) \rangle$.

ACKNOWLEDGMENTS

We acknowledge support from the Army Research Laboratory under Grant No. W911NF-17-1-0164 (C.O.), NSF Grants No. CBET-2002782 (C.O.) and No. CBET-2002797 (M.S.), and China Scholarship Council Grant No. 201906340202 (S.Z.). This work was also supported by the High Performance Computing facilities operated by Yale's Center for Research Computing and computing resources provided by the Army Research Laboratory Defense University Research Instrumentation Program Grant No. W911NF-18-1-0252.

APPENDIX: AFFINE SHEAR MODULUS

In Sec. III C in the main text, we calculated the nonaffine shear modulus $G_{na} = G - G_a$ for low-pressure geometrical families for jammed packings of circulo-lines. In this Appendix, we derive an expression for the affine contribution to the shear modulus, G_a , for jammed packings of circulo-lines. For a globally affine simple shear strain, the particle positions and orientations of each circulo-line change according to Eqs. (3) and (4), and the affine contribution to the shear stress is

$$\Sigma_a = L^{-2} \frac{dU(r_{ij})}{d\gamma}, \quad (\text{A1})$$

where the contact distance vector satisfies

$$\vec{r}_{ij} = \vec{c}_{ij} + \lambda_j \hat{u}_j - \lambda_i \hat{u}_i, \quad (\text{A2})$$

$\vec{c}_{ij} = (x_{ij}, y_{ij})$ is the the separation vector between the centers of mass of particles i and j , and $\hat{u}_i = (\cos \theta_i, \sin \theta_i)$. We set $\lambda_i = l_i$ and $\lambda_j = l_j$ for end-end contacts and set

$$\lambda_i = (\vec{r}_{ij} + \lambda_j \hat{u}_j) \cdot \hat{u}_i \quad (\text{A3})$$

for end-middle contacts, where $\lambda_j = l_j$ and particle j is the particle whose end is in contact with the middle section of particle i .

The affine shear modulus is

$$G_a = \frac{d\Sigma_a}{d\gamma} = L^{-2} \frac{d^2U(r_{ij})}{d\gamma^2}. \quad (\text{A4})$$

Using Eq. (1), we obtain the following for the second derivative of the total potential energy with respect to shear strain γ :

$$\frac{d^2U(r_{ij})}{d\gamma^2} = \frac{1}{\sigma_{ij}^2} \left(\left(\frac{dr_{ij}}{d\gamma} \right)^2 - (\sigma_{ij} - r_{ij}) \frac{d^2r_{ij}}{d\gamma^2} \right). \quad (\text{A5})$$

For both end-end and end-middle contacts, the first and second derivatives of the contact distance with strain are given by

$$\frac{dr_{ij}}{d\gamma} = \frac{f_1 x_{ij} + f_2 y_{ij}}{r_{ij}} \quad (\text{A6})$$

and

$$\frac{d^2r_{ij}}{d\gamma^2} = -\frac{(f_1 x_{ij} + f_2 y_{ij})^2}{r_{ij}^3} + \frac{f_1^2 + f_2^2 + f_3 x_{ij} + f_4 y_{ij}}{r_{ij}}, \quad (\text{A7})$$

respectively, where f_1, f_2, f_3 , and f_4 are functions of $\lambda_i, \lambda_j, \theta_i$, and θ_j . For end-end contacts,

$$f_1 = y_{ij} - \lambda_i \sin^3 \theta_i + \lambda_j \sin^3 \theta_j, \quad (\text{A8})$$

$$f_2 = \lambda_i \sin^2 \theta_i \cos \theta_i - \lambda_j \sin^2 \theta_j \cos \theta_j, \quad (\text{A9})$$

$$f_3 = 3\lambda_i \sin^4 \theta_i \cos \theta_i - 3\lambda_j \sin^4 \theta_j \cos \theta_j, \quad (\text{A10})$$

and

$$f_4 = (3 \sin^2 \theta_i - 2) \cos \theta_i - (3 \sin^2 \theta_j - 2) \cos^2 \theta_j. \quad (\text{A11})$$

For end-middle contacts, f_1, f_2, f_3 , and f_4 obey different expressions. We find

$$f_1 = y_{ij} - \lambda_i \sin^3 \theta_i + \lambda_j \sin^3 \theta_j + f_5 \cos \theta_j, \quad (\text{A12})$$

$$f_2 = \lambda_i \sin^2 \theta_i \cos \theta_i - \lambda_j \sin^2 \theta_j \cos \theta_j + f_5 \sin \theta_j, \quad (\text{A13})$$

$$f_3 = 3\lambda_i \sin^4 \theta_i \cos \theta_i - 3\lambda_j \sin^4 \theta_j \cos \theta_j + 2f_5 \sin^3 \theta_j + f_6 \cos \theta_j, \quad (\text{A14})$$

and

$$f_4 = (3 \sin^2 \theta_i - 2) \cos \theta_i - (3 \sin^2 \theta_j - 2) \cos^2 \theta_j - 2f_5 \sin^2 \theta_j \cos \theta_j + f_6 \sin \theta_j, \quad (\text{A15})$$

where

$$f_5 = (y_{ij} + \lambda_j \sin^3 \theta_j) \cos \theta_i + (x_{ij} + \lambda_j \cos \theta_j) \sin^3 \theta_i - \lambda_j \sin^2 \theta_j \cos \theta_j / \sin \theta_i - (y_{ij} + \lambda_j \sin \theta_j) \sin^2 \theta_i \cos \theta_i \quad (\text{A16})$$

and

$$f_6 = -3\lambda_j \cos \theta_i \sin^4 \theta_j \cos \theta_j \\ + 2(y_{ij} + \lambda_j \sin^3 \theta_j) \sin^3 \theta_i \\ - 3(x_{ij} + \lambda_j \cos \theta_j) \sin^4 \theta_i \cos \theta_i$$

$$- \lambda_j \sin^3 \theta_j (3 \sin^2 \theta_j - 2) \sin \theta_i \\ + 2\lambda_j \sin^2 \theta_j \cos \theta_j \sin^2 \theta_i \cos \theta_i \\ - (y_{ij} + \lambda_j \cos \theta_j) \sin^3 \theta_i (3 \sin^2 \theta_i - 2). \quad (\text{A17})$$

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